


# Eurocode 1: Actions on structures –

Part 1–2: General actions –  
Actions on structures exposed to fire

**Annex A** (informative)


→ Parametric temp-time curves

Part of the One Stop Shop program



## Introduction

- Method of determining a **more realistic** temperature-time curve
- Valid for compartments
  - Up to 500m<sup>2</sup> of floor area
  - Without openings in roof
  - Up to 4m in height




## Basic fundamental equation

- Temperature-time curves in **heating** phase are given by:

$$\Theta_g = 20 + 1325 \cdot (1 - 0.324e^{-0.2t^*} - 0.204e^{-1.7t^*} - 0.472e^{-19t^*})$$

where  $\Theta_g$  is the gas temperature in the fire compartment

- The “time”  $t^*$  is not strictly the time, but an adjusted time based on other factors



## Breaking down the equation

$$t^* = t \cdot \Gamma$$

$$\Gamma = \frac{(O/b)^2}{(0.04/1160)^2}$$


$$b = \sqrt{(\rho c \lambda)}$$

$$O = \frac{A_v \sqrt{h_{eq}}}{A_t}$$

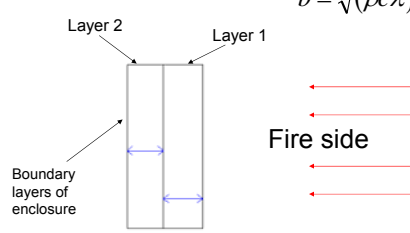
(\*Opening factor\*)

$\rho$  – Density of enclosure boundary  
 $C$  – Specific heat of enclosure boundary  
 $\lambda$  – Thermal conductivity of enclosure boundary  
 $A_v$  – Total area of vertical openings on walls  
 $h_{eq}$  – Weighted average of window heights on all walls  
 $A_t$  – Total area of enclosure (incl. openings)

This outlines the basis of the equation used  
Further details of limitations and further provisos are also necessary.....




## Different materials in surface layer



$$b = \sqrt{(\rho c \lambda)}$$

For layer 1, the subscript <sub>1</sub> is used and similarly for layer 2.....



## Different materials in surface layer

$$b = \sqrt{(\rho c \lambda)}$$

- If  $b_1 < b_2$ , then  $b = b_1$
- If, however,  $b_1 > b_2$  then a **limit thickness** is calculated for the **exposed** material:

$$s_{lim} = \sqrt{\frac{3600 \cdot t_{max} \cdot \lambda_1}{c_1 \rho_1}}$$

(We will find an expression for  $t_{max}$  in a few slides time...)

If  $s_1 > s_{lim}$ , then  $b = b_1$

If  $s_1 < s_{lim}$ , then  $b = \frac{s_1}{s_{lim}} b_1 + \left(1 - \frac{s_1}{s_{lim}}\right) b_2$

**Different materials in surface layer**

$$b = \sqrt{(\rho c \lambda)}$$

- To account for the different  $b$  factors in the walls, the above equation should be introduced as

$$b = \frac{\sum (b_j A_j)}{A_t - A_v}$$

Where  $A_j$  is the area of the surface enclosure and  $b_j$  is the  $b$  factor derived from the previous slide

**Maximum temperature limit**

- The **maximum temperature** in the heating phase occurs when  $t^* = t_{\max}^*$

at which point  $t_{\max}^* = t_{\max} \cdot \Gamma$

with  $t_{\max} = \max \left[ \left( \frac{2 \times 10^{-4} \cdot q_{t,d}}{O} \right); t_{\lim} \right]$

Where.....

**Maximum temperature limit**

- $q_{t,d}$  is the **design value of the fire load density related to the area of the enclosure**

$$q_{t,d} = q_{f,d} \cdot \frac{A_f}{A_t}$$

Design value of fire load density related to surface area of the floor – from Annex E

Surface area of the floor

Total surface area of compartment

- $t_{\lim}$  is described later.....

**Maximum temperature limit**

- When  $t_{\max} = t_{\lim}$  the  $t^*$  in the main equation is replaced by  $t^* = t \cdot \Gamma_{\lim}$

$$\text{with } \Gamma_{\lim} = \frac{(O_{\lim} / b)^2}{(0.04 / 1160)^2}$$

where  $O_{\lim} = \frac{1 \times 10^{-4} \cdot q_{t,d}}{t_{\lim}}$

$t_{\lim}$  is 25min for **slow** fire growth, 20min for **medium** fire growth and 15min for **fast** fire growth.

This is expanded upon in Annex E

**Further numerical limit**

- A further limit is imposed on the operation under the following criteria:

If  $O > 0.04$   
and  $q_{t,d} < 75$   
and  $b < 1160$

Then  $\Gamma_{\lim}$  must be multiplied by a **factor** given below....

$$k = 1 + \left( \frac{O - 0.04}{0.04} \right) \left( \frac{q_{t,d} - 75}{75} \right) \left( \frac{1160 - b}{1160} \right)$$

**Curves in the cooling phase**

- For  $t_{\max}^* \leq 0.5$

$$\Theta_g = \Theta_{\max} - 625(t^* - t_{\max}^* \cdot x)$$


Where

$t^* = t \cdot \Gamma$

For  $t_{\max} > t_{\lim}$  →  $x = 1$

For  $t_{\max} = t_{\lim}$  →  $x = \frac{t_{\lim} \cdot \Gamma}{t_{\max}^*}$

$t_{\max}^* = \left( \frac{2 \times 10^{-4} \cdot q_{t,d}}{O} \right) \cdot \Gamma$



### Curves in the cooling phase

- For  $0.5 < t_{\max}^* < 2$

$$\Theta_g = \Theta_{\max} - 250(3 - t_{\max}^*) \cdot (t^* - t_{\max}^* \cdot x)$$


Where

$$t_{\max}^* = \left( \frac{2 \times 10^{-4} \cdot q_{t,d}}{O} \right) \cdot \Gamma$$

For  $t_{\max} > t_{\lim}$   $\longrightarrow x = 1$

For  $t_{\max} = t_{\lim}$   $\longrightarrow x = \frac{t_{\lim} \cdot \Gamma}{t_{\max}^*}$

$t^* = t \cdot \Gamma$



### Curves in the cooling phase

- For  $t_{\max}^* \geq 2$

$$\Theta_g = \Theta_{\max} - 250(t^* - t_{\max}^* \cdot x)$$

Where

$$t^* = t \cdot \Gamma$$

$$t_{\max}^* = \left( \frac{2 \times 10^{-4} \cdot q_{t,d}}{O} \right) \cdot \Gamma$$

For  $t_{\max} > t_{\lim}$   $\longrightarrow x = 1$

For  $t_{\max} = t_{\lim}$   $\longrightarrow x = \frac{t_{\lim} \cdot \Gamma}{t_{\max}^*}$